

NLC - The Next Linear Collider Project



Renewable & Consumable Collimators at the NLC

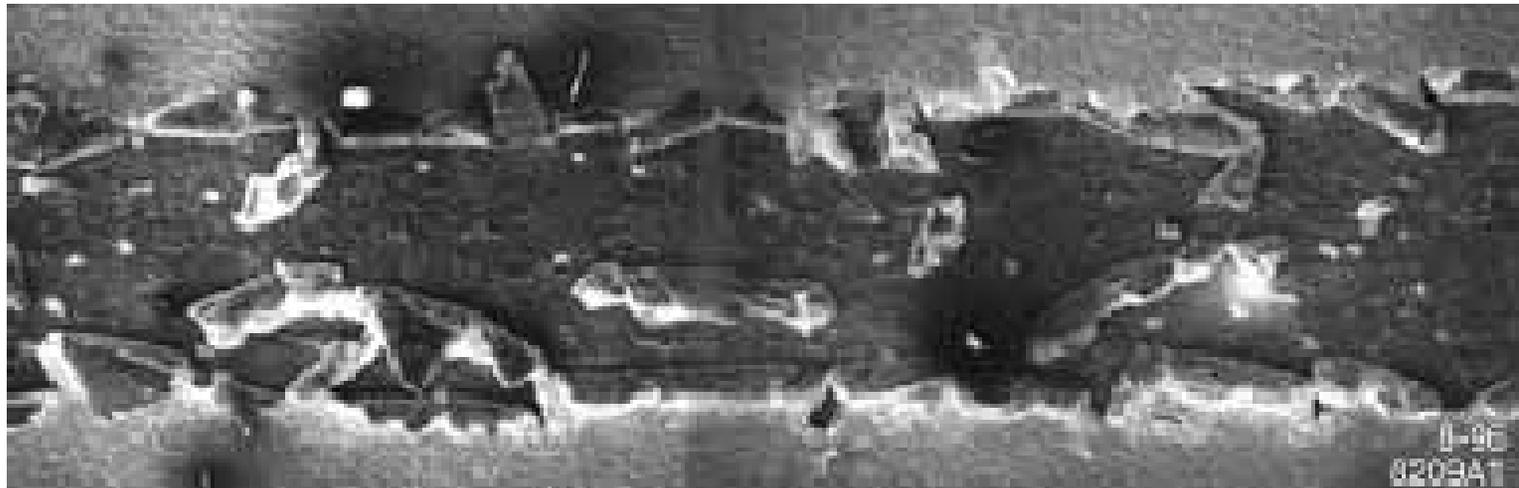
Eric Doyle, Josef Frisch, Tom Markiewicz, Knut Skarpaas VIII
SLAC

Halo '03 Montauk NY
22 May 2003



Collimator Damage

SLC Linac Collimators in 1995: Gold-coated Titanium

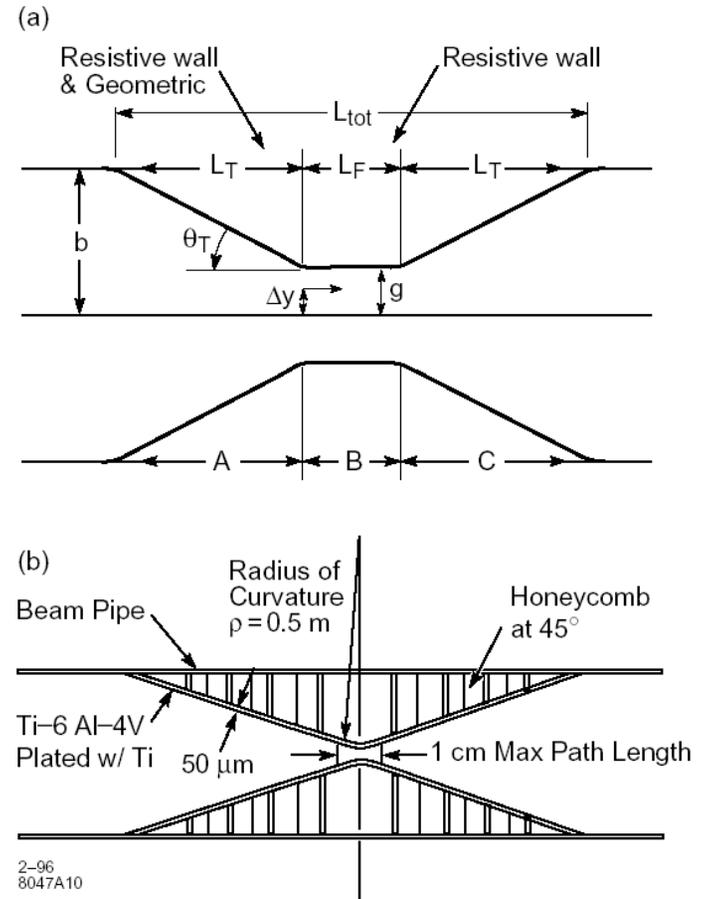
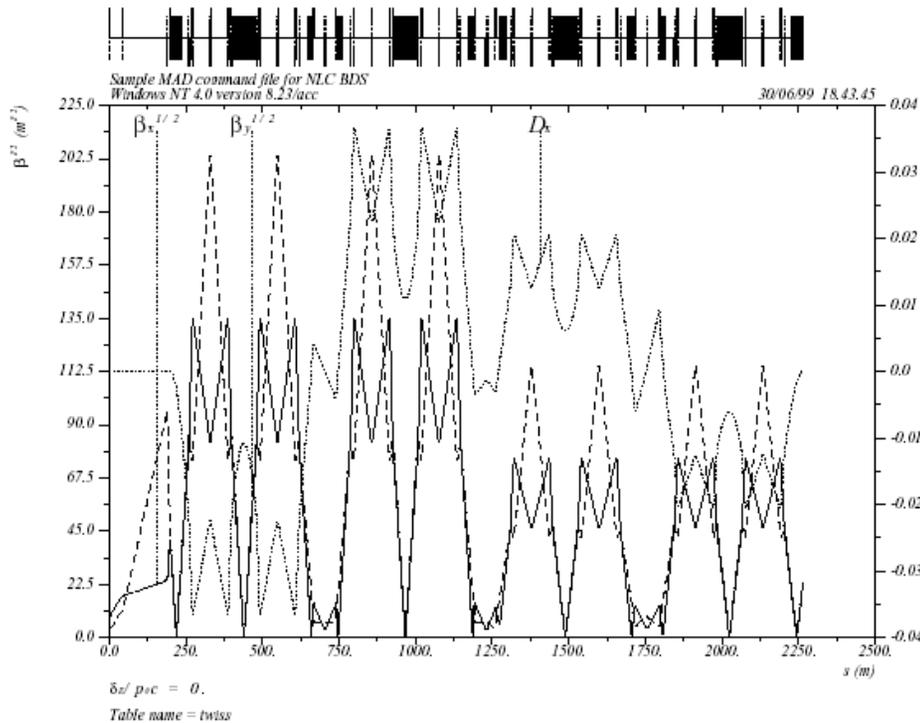


1mm

Feature size $\sim 250\mu\text{m}$

Wakefields $\times 25-50$ larger than before damage

1996 NLC ZDR Collimation Lattice based on thin spoilers and thick absorbers



- Large betatron function
- Large dispersion
- Large separation between spoilers and absorbers



PASSIVE Protection Makes for SENSITIVE Lattice

- Long system length (~ 2.5 km per side)
- Several interleaved families of sextupoles for chromatic correction
 - Small bandwidth
 - Tight tolerances, particularly sextupole alignment
- Large $R_{12,34}$ elements from one sector to the next
 - Diurnal Quad Drift of a few μm in one sector would drive the beam into the collimators in the next sector, damaging downstream absorbers
- Interleaved Horizontal Betatron and Energy collimation
 - Many collimators
 - No additional spoilers could be added
 - Wakefields from the collimators were at the limit of tolerability
 - Horizontal collimation depth could not be adjusted independently of the energy collimation depth
- Looser IP- vs. FD-phase collimation in the 2nd pass (strong wakes)
 - Careful control of phase advance, both for on- and off-energy particles, to prevent phase migration
 - Careful control of the chromaticity

Damageable Collimators Share Pain

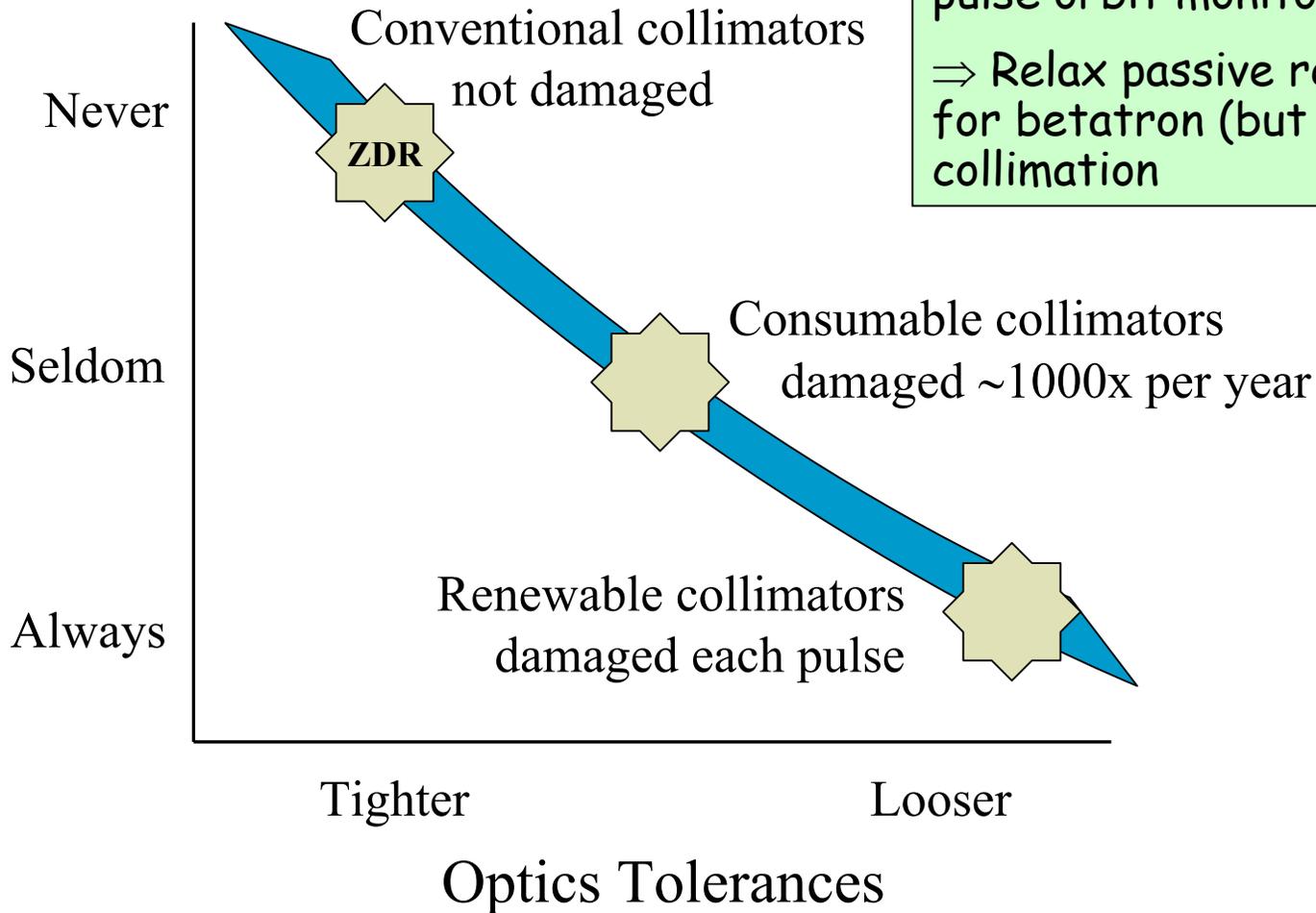
SLC experience

- Frequent energy errors &/or feedback system problems
- Few catastrophic quad failures

NLC MPS requires pulse-to-pulse orbit monitoring

⇒ Relax passive requirement for betatron (but not energy) collimation

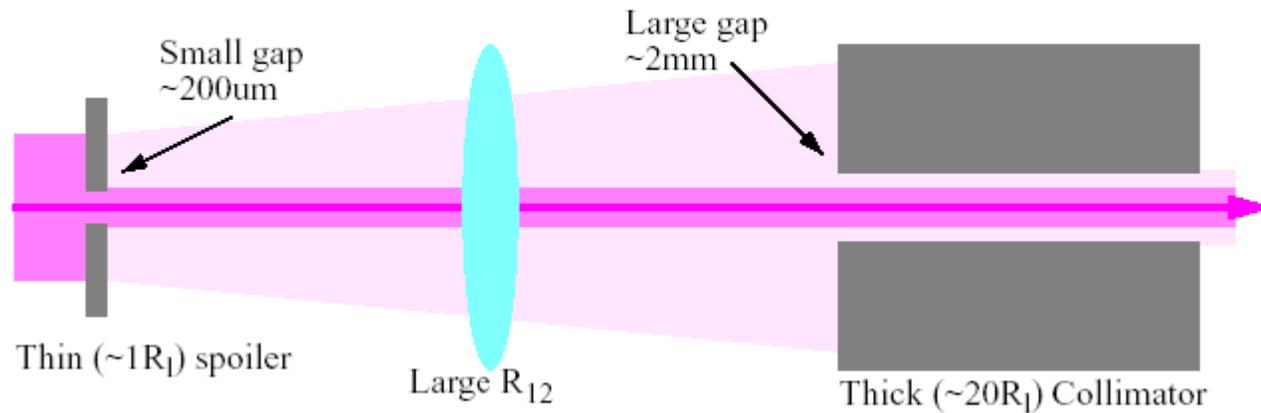
Single Pulse Collimator Damage





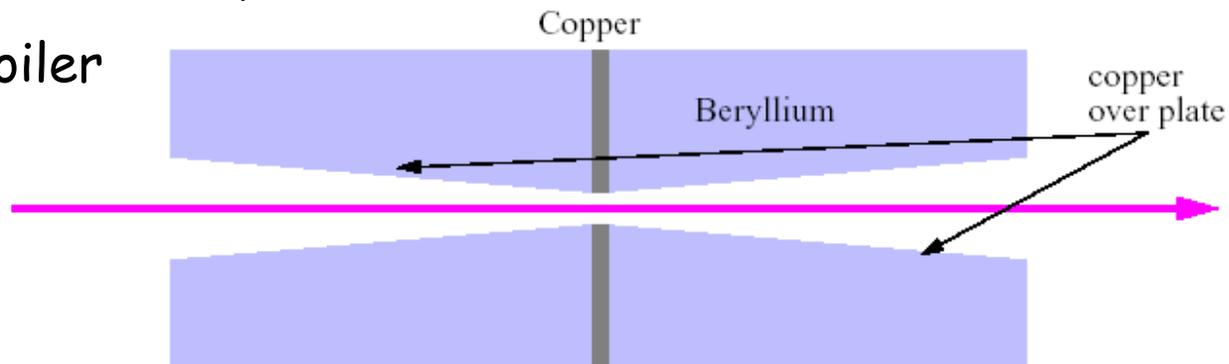
Consumable/Renewable Spoilers

Spoiler / Absorber Scheme



Tapered low resistivity surface for wakefields

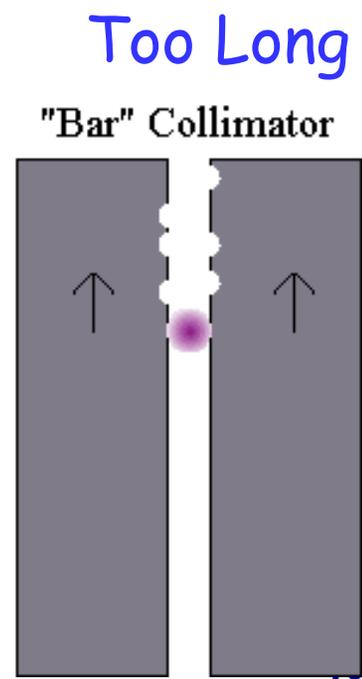
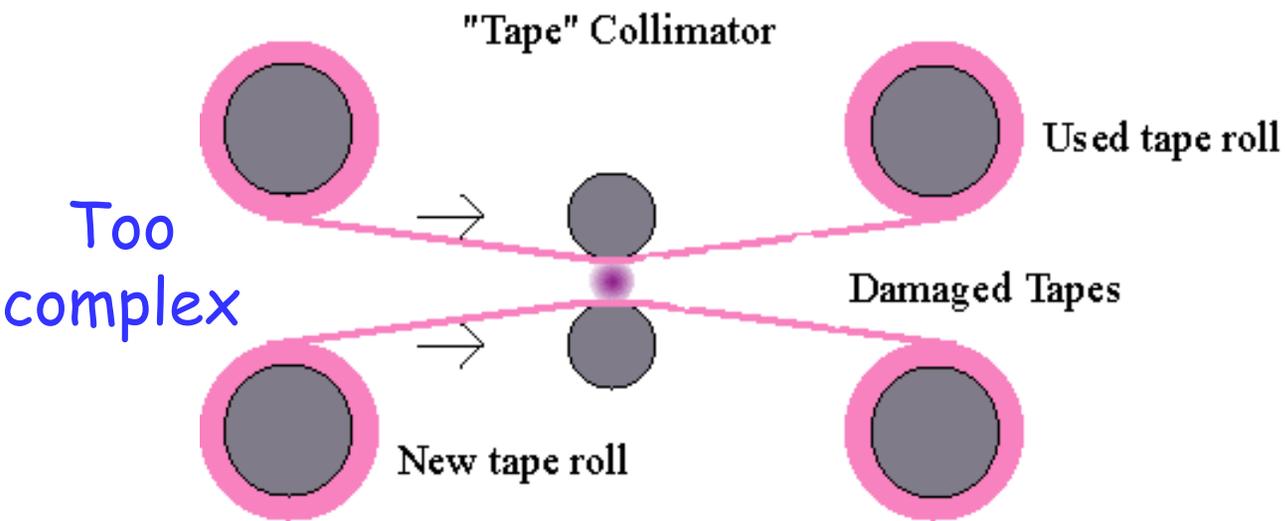
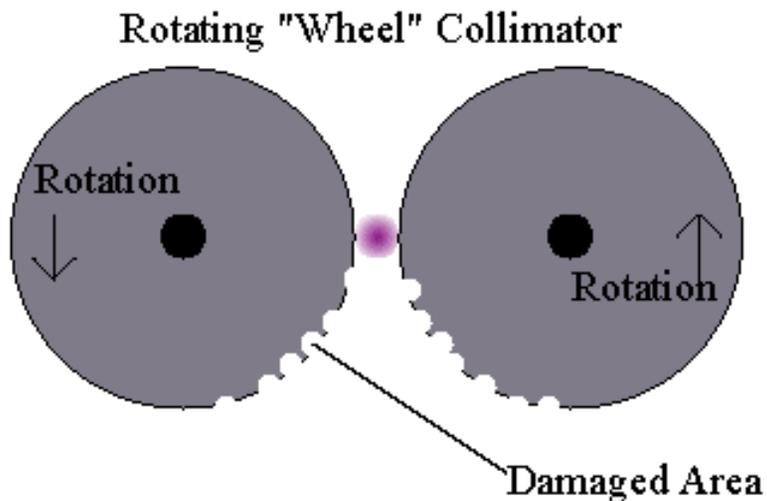
Thin hi-Z spoiler





Consumable Options Considered

Option Chosen





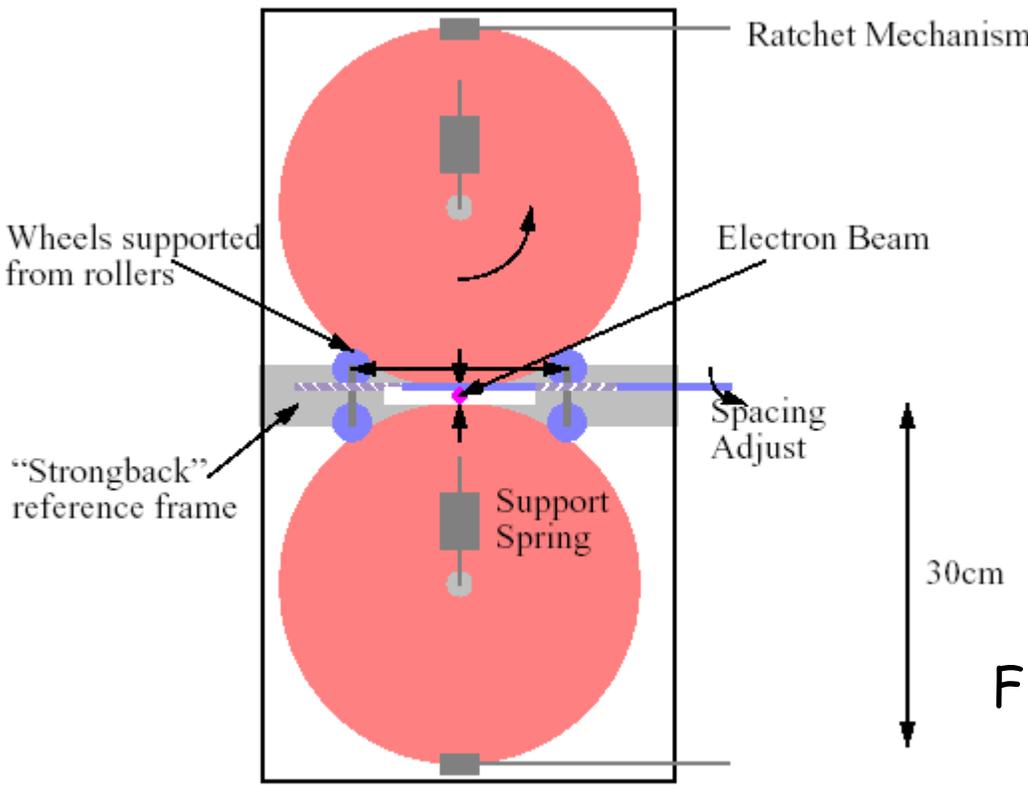
Consumable Spoiler Requirements

Max.# Damaging Hits	1000
Length @ Min. Gap	0.6 rl
Radius of curvature	.5 m
Aperture	200-2000 μm
Edge Placement Accuracy	10-20 μm
Edge Stability under rotation	5 μm
Beam Pipe ID	10 mm
% Beam Intercepted per side	.05%
Beam Halo Heating	~0.2 W
Image Current Heating	~0.5 W
Radiation Environment	10^5-10^6 rad/hour
Vacuum (tbd)	$<10^{-7}$ torr

~30cm
diameter

Radiative
Cooling

Rotating Wheel Design Features



1 d.o.f. internal mechanism
referenced to rigid backplane
provides aperture

Control through transversely
adjustable stops

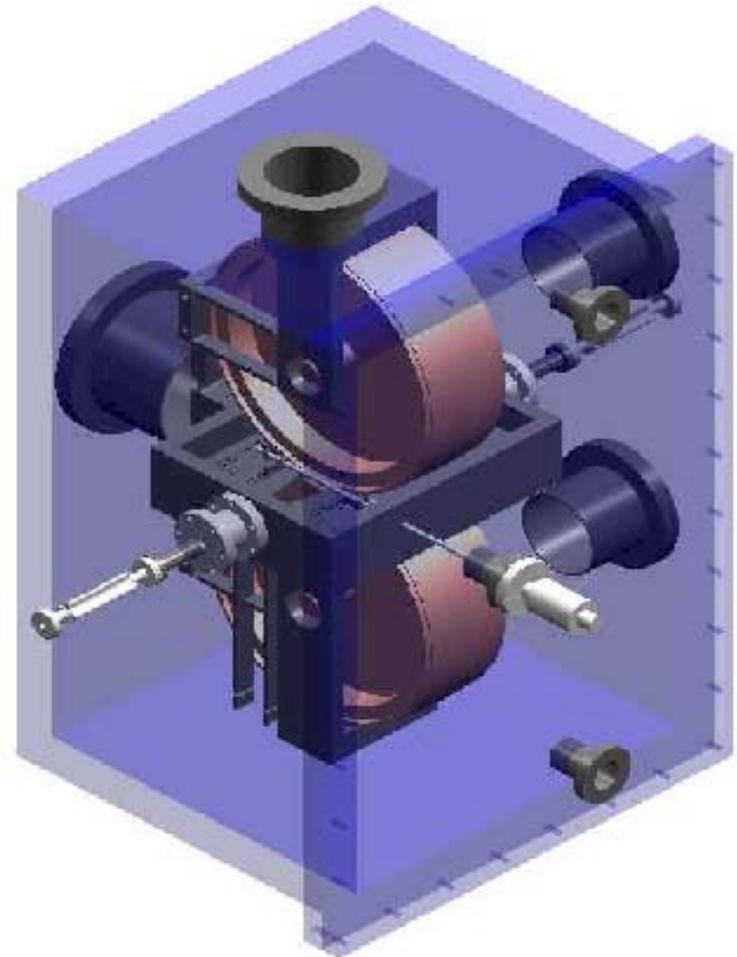
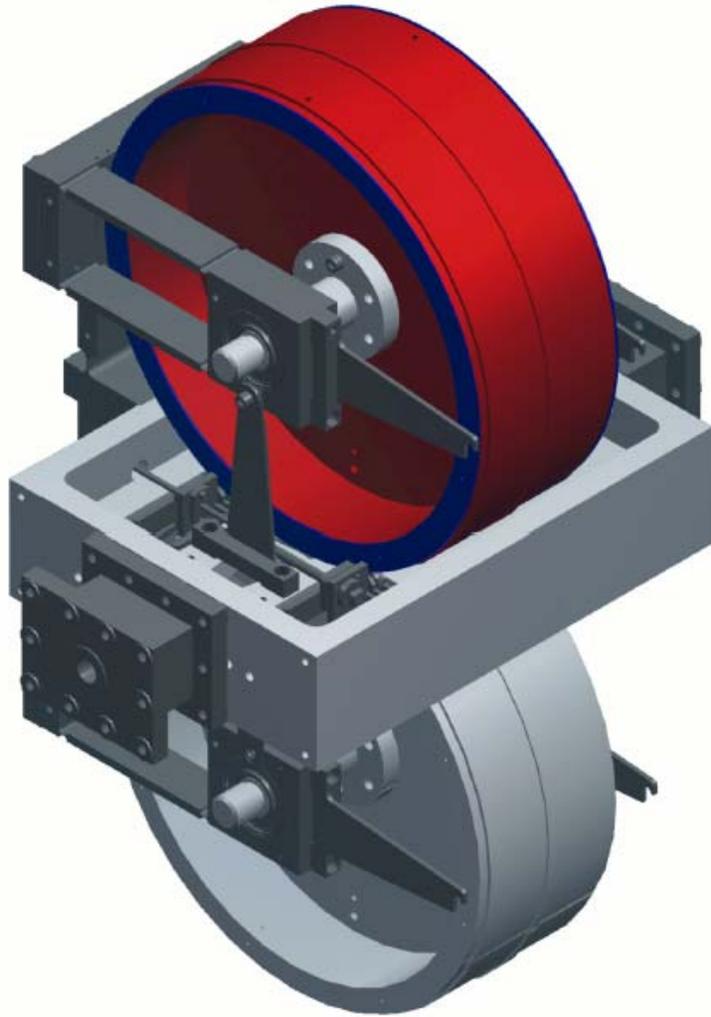
Flexure pivots eliminate backlash

Vacuum bearings

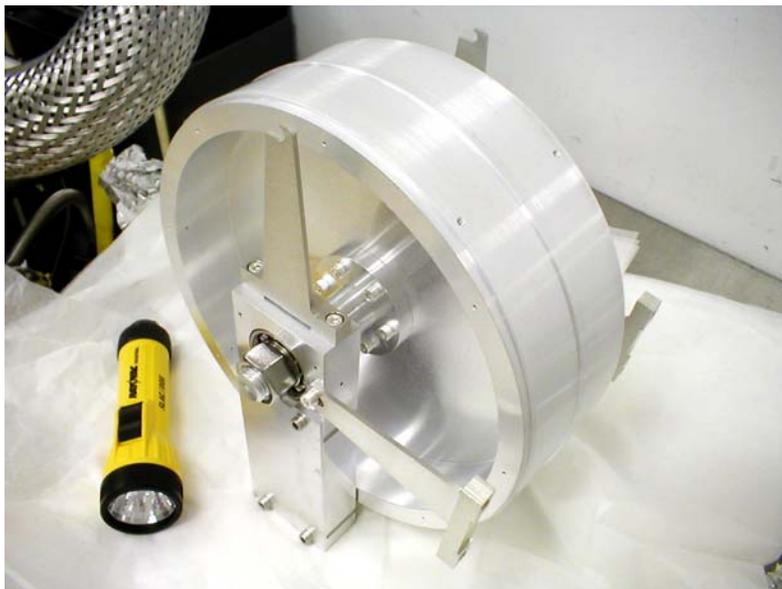
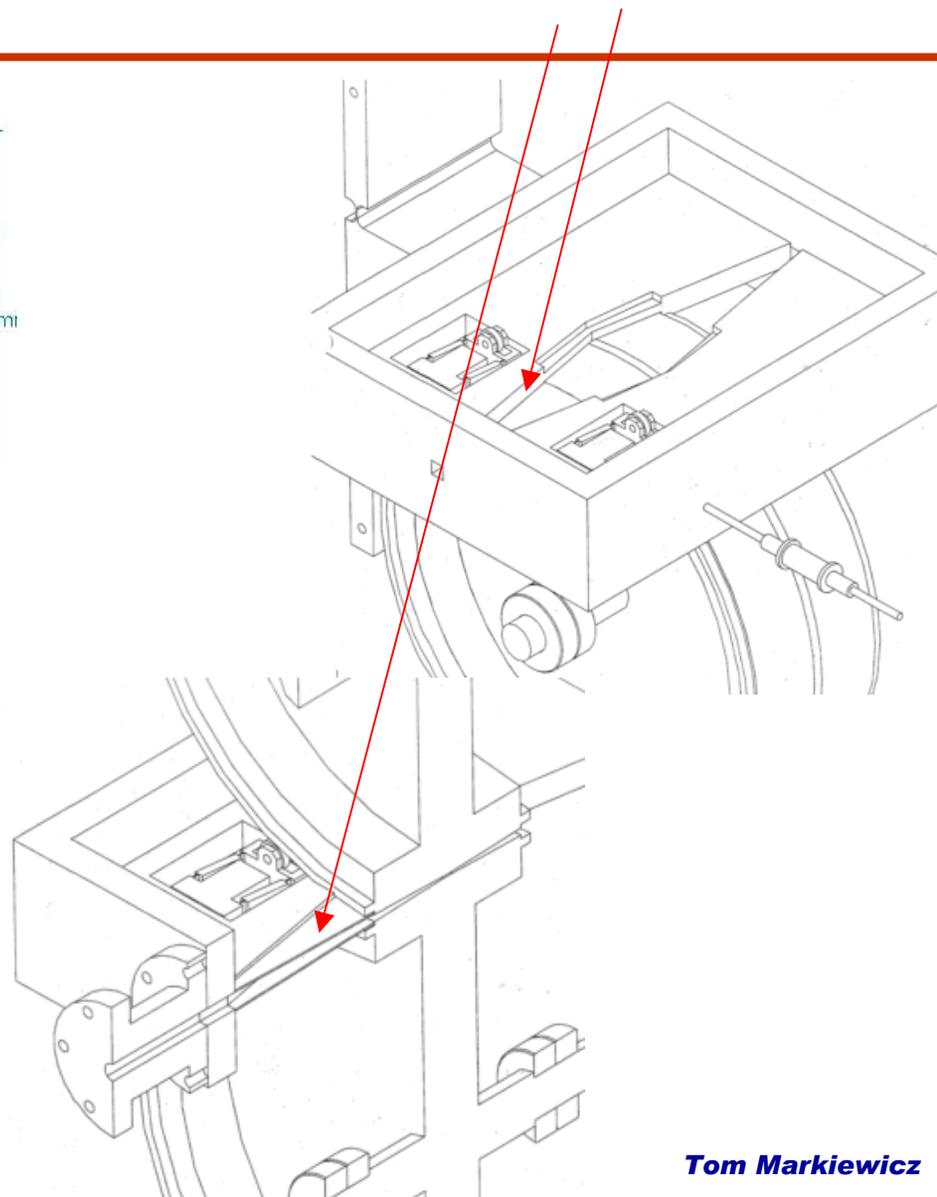
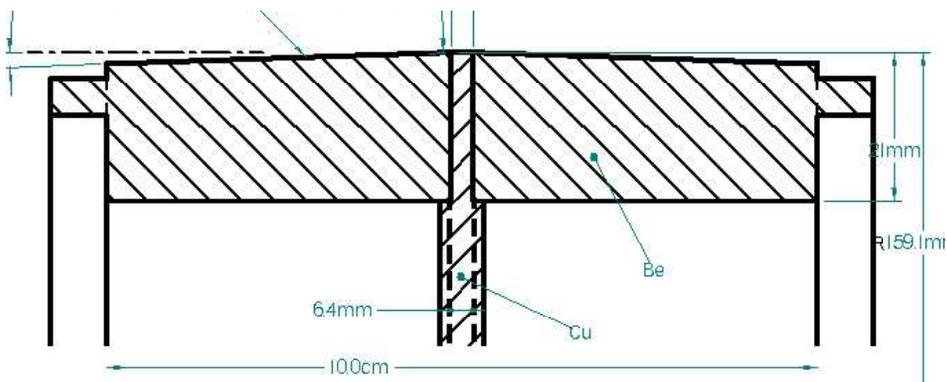
Housing aligned to beam via
external movers & BPMs

Engineer to minimize thermal
effects

Consumable Spoiler Prototype

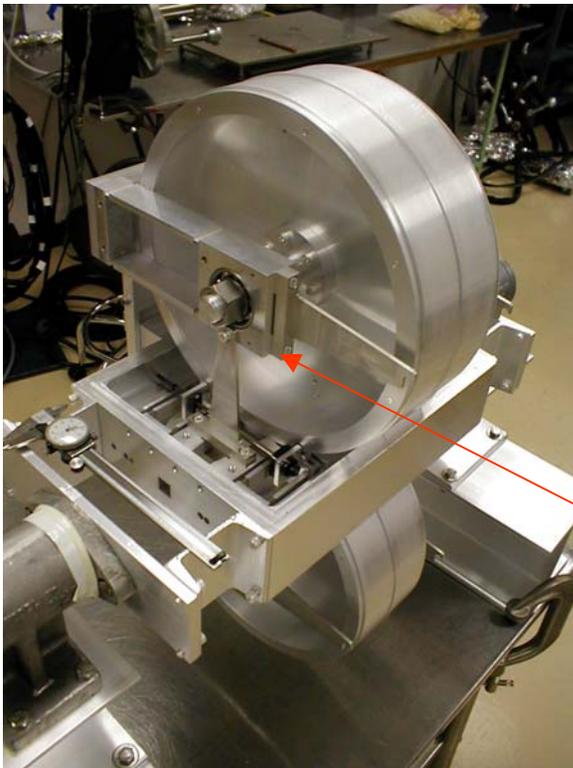
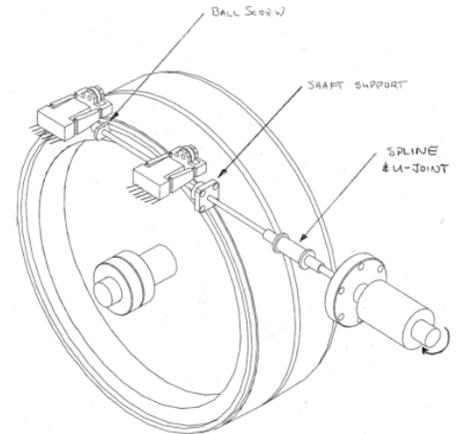
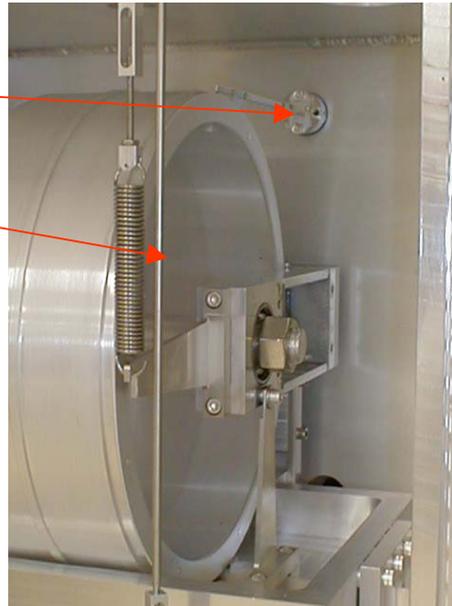


Tapered Wheels & Wakefield Wedges

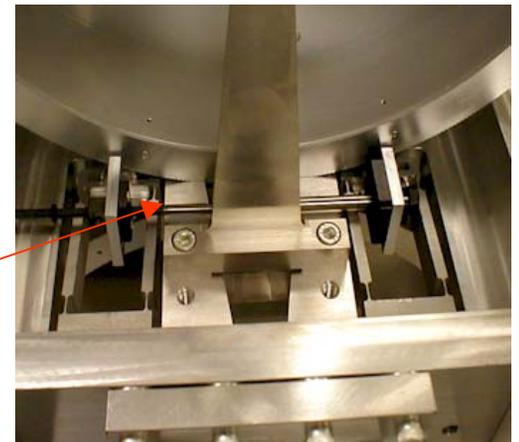


Adjustment Mechanisms

Wheel Ratchet
& Support



Aperture Adjust



Mounted in Vacuum Vessel

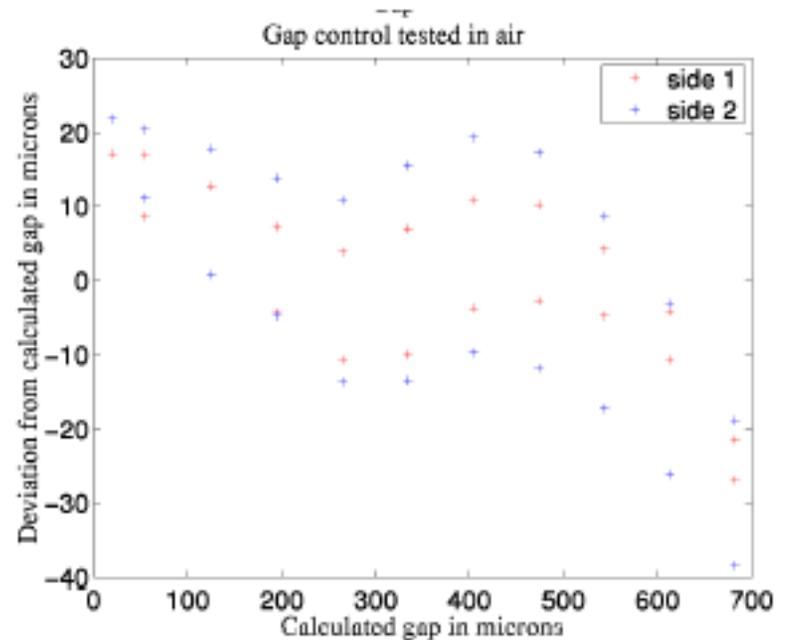
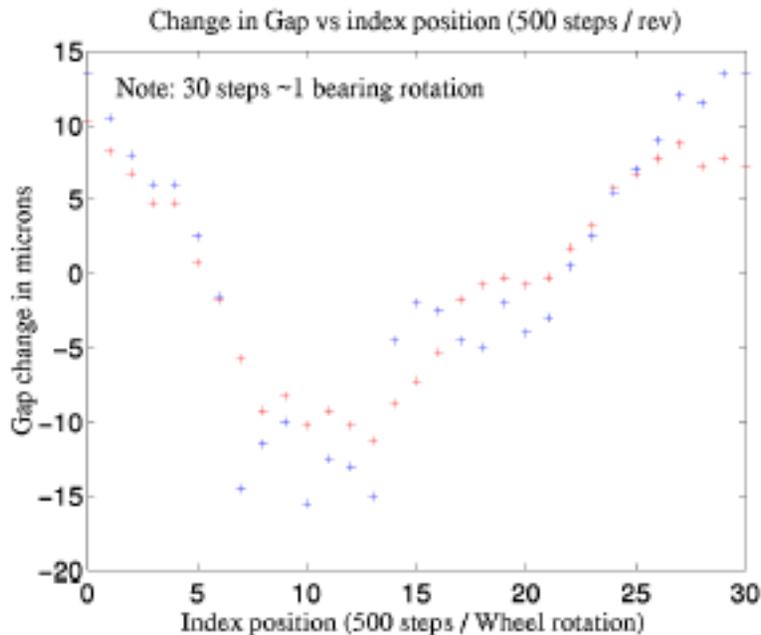


Consumable Spoiler Performance (1)

Stability with Wheel Rotation
 $\sim \pm 15 \mu\text{m}$

Runout in support bearings;
Use higher precision bearings

Motion accuracy $\sim \pm 15 \mu\text{m}$
OK





Consumable Spoiler Performance (2)

- Hysteresis in Gap as Wheel Rotated $\sim 25 \mu\text{m}$
 - Improve by reducing torque from support springs
- Vacuum 2×10^{-7} torr
- Heat performance

3.5W/rotor	10W/rotor	11W/rotor
$\Delta T=17^\circ\text{C}$	$\Delta T=42^\circ\text{C}$	$\Delta T=46^\circ\text{C}$
5/250 μm	8/250 μm	15/250 μm

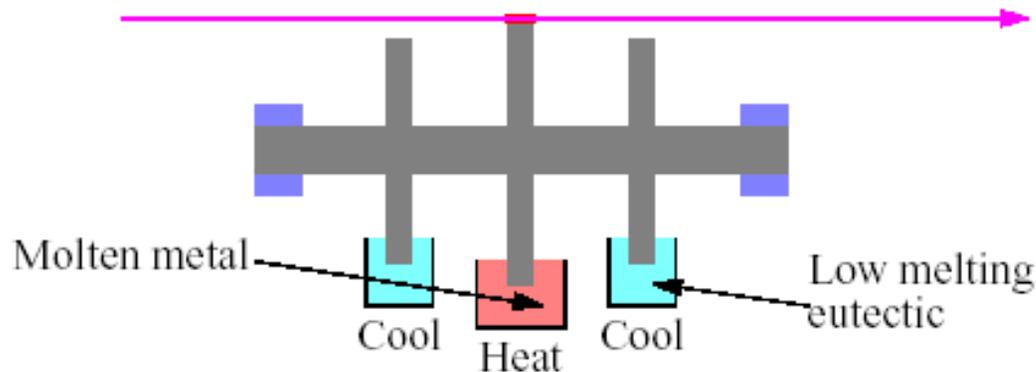
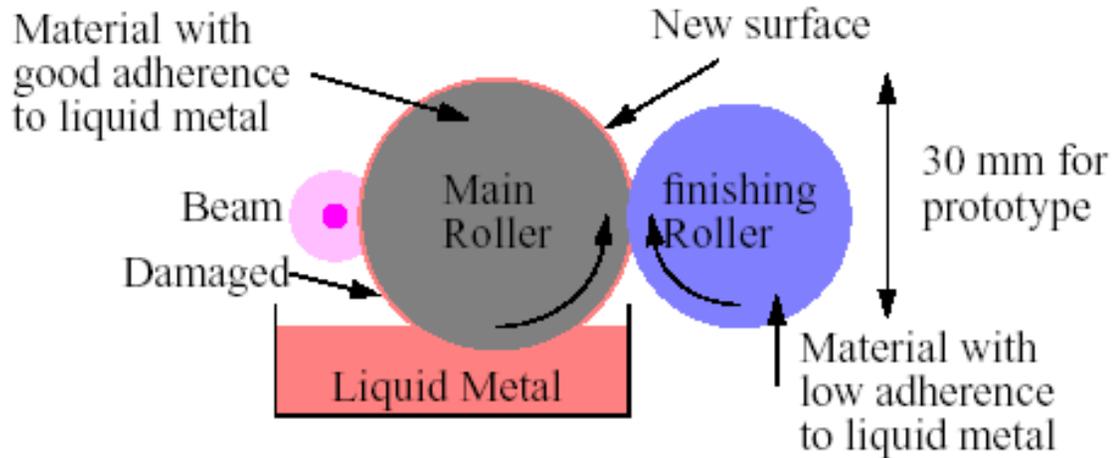


Consumable Collimators at LHC?

- Minimum required jaw length for Be, C, Ti, Cu, W?
- Allowable impedance for each of the above?
- Maximum anticipated steady-state design power deposited?
- Maximum allowed radiation dose level in the collimation section 30cm from the beamline. To what extent must radiation hard materials be used?
- Vacuum requirements in the collimators? $1\text{E}-6$ torr (easy), or $1\text{E}-10$ torr (will required special materials).
- What is the separation between the two beams, and can they be run through the same chamber?
- Any other unusual constraints? Nonmagnetic materials? Low activation materials?...
- Reliability requirements? Obviously very high. Is there space for dual collimators?

Renewable Spoilers

Solidifying metal system - one side shown



Advantages:

- Very Small Gap relaxes optics tolerances
- No need to ask if surface is damaged or not



Materials Studies

- **Which liquid metal?** TIN
 - low vapor pressure at its melting point
 - Indium is a possible alternate
- **Smoothing roller material?** Molybdenum
 - not coated or corroded by hot Tin
 - Tungsten is better but more difficult to machine.
- **Main spoiler wheel material** Tin-coated Niobium
 - **Most difficult requirement: Need a material which can be repeatedly coated with but which will not dissolve**
 - Metal coatings (i.e. soldering) dissolve outer surface of substrate
 - Solution: "Pre-treat" the substrate material in liquid Tin at high temperature (850 °C) for 24 hours. This dissolves the outer portion of the substrate and forms a good coating. Then operate the roller in low temperature liquid Tin (280 °C). At this lower temperature the dissolving rate is vanishingly small.



Liquid Metal Properties

Material	Melting Point C	Vapor Pressure MP/ MP+100C Torr	Radiation Length cm
Li	180	$10^{-10}/10^{-7}$	150
Ga	30	$<10^{-11}/<10^{-11}$	2.1
In	156	$<10^{-11}/<10^{-11}$	1.2
Sn	231	$<10^{-11}/<10^{-11}$	1.2
Tl	303	$10^{-8}/10^{-6}$	0.5
Pb	327	$10^{-8}/10^{-6}$	0.6
Bi	271	$10^{-10}/10^{-7}$	0.6

Desirable Properties:

Pure element

Low vapor pressure

Short Radiation Length

Tin chosen as indium
activates and shows
inferior adherence
relative to tin

Substrate Materials

Goal: Corrosion free with good adherence

TESTED:

Beryllium: Long radiation length is an advantage

Carbon: Pyrolytic Graphite very corrosion resistant, long rad. length

Silicon: Corrosion resistant.

Titanium: Good mechanical properties, corrosion resistant.

Vanadium: Corrosion resistant

Iron: Resistant to some liquid metals. Cheap and easy to work with

Zirconium: Generally corrosion resistant.

Molybdenum: Corrosion resistant, high temperature

Tantalum: Corrosion resistant, high temperature

Tungsten: Very high temperature, corrosion resistant.

Stainless steel: Resistant to some liquid metals. Cheap, easy to work with.

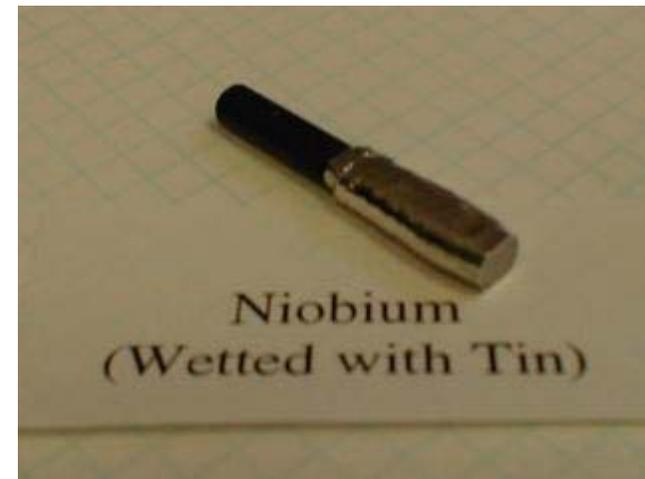
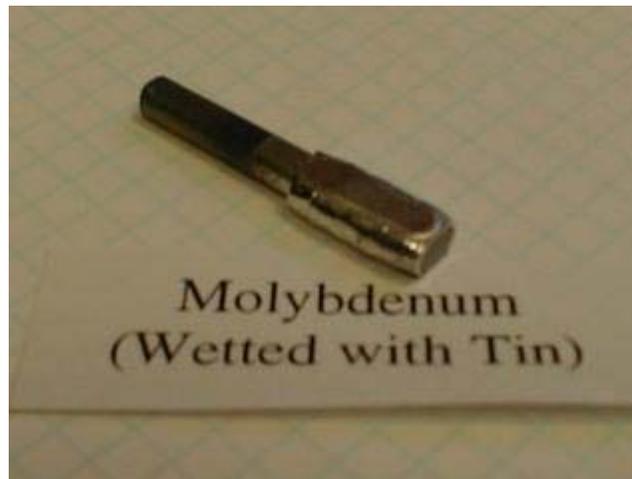
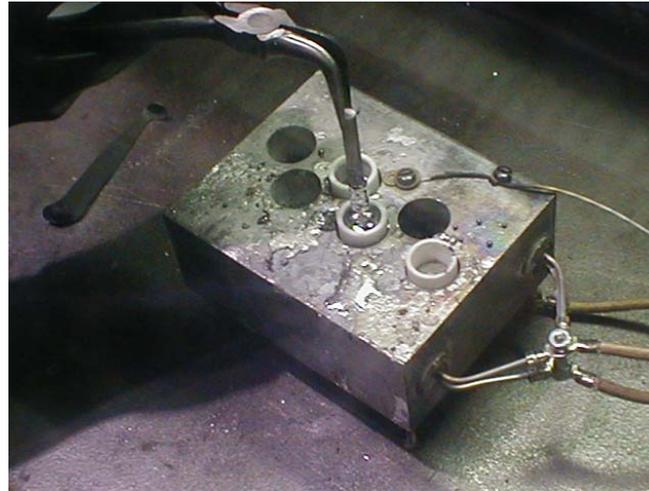
Aluminum Oxide (ceramic): Corrosion resistant

Tungsten Carbide (ceramic): Corrosion resistant, high temperature.

Materials R&D



Glove Box under
N₂



Liquid Metal/Substrate Tests

Goal: Corrosion free with good adherence

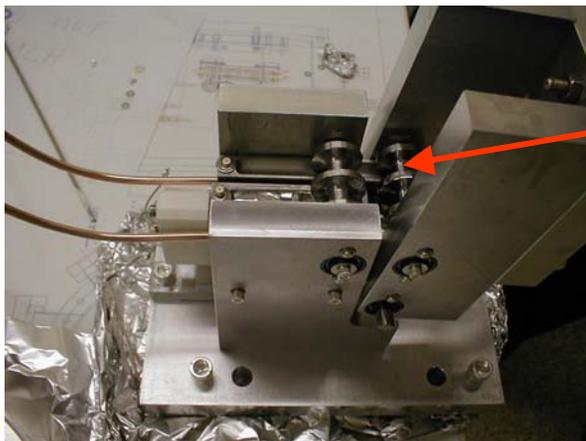
400°C Tests with Sn (under N₂):

- No adherence for any substrate except iron
- Iron "wets" at 400 °C then continues down to 231 °C
- Nickel-coated steel, Silver-coated stainless:
 - coatings dissolve, then no adherence

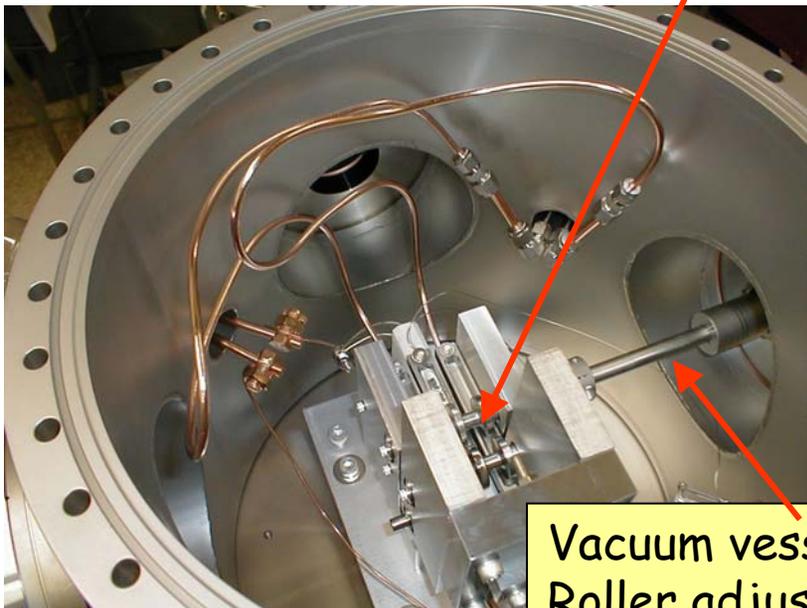
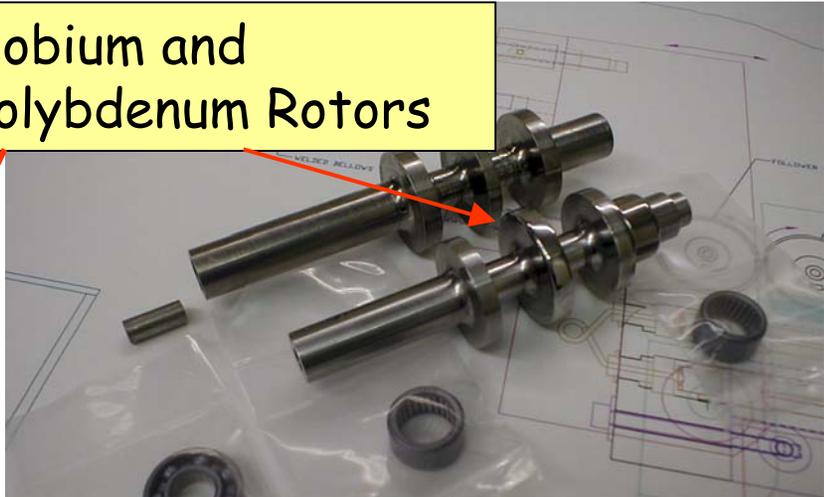
800°C Tests (under N₂):

- Nickel, Zirconium, Aluminum, Steel, Iron, Silicon, Silver, Titanium, Tungsten Carbide: dissolve, distort &/or corrode
- Tungsten, Glassy Carbon, Aluminum oxide, Beryllium: No adherence
- **Molybdenum: Adherence, which then continues at lower T, no sign of corrosion after 5 days at 380 °C ; Use as roller**
- Tantalum: Adherence, continuation at lower T, then de-wets; sample reacts with N₂; suspect dissolved N₂ in Sn sample
- Vanadium: Adherence, but with mild corrosion; continuation at lower T without further corrosion
- Rhenium: Similar to Moly, but expensive
- **Niobium: Wets & slightly dissolves at 850 °C; stable at 300 °C for several weeks; Use as main rotor**

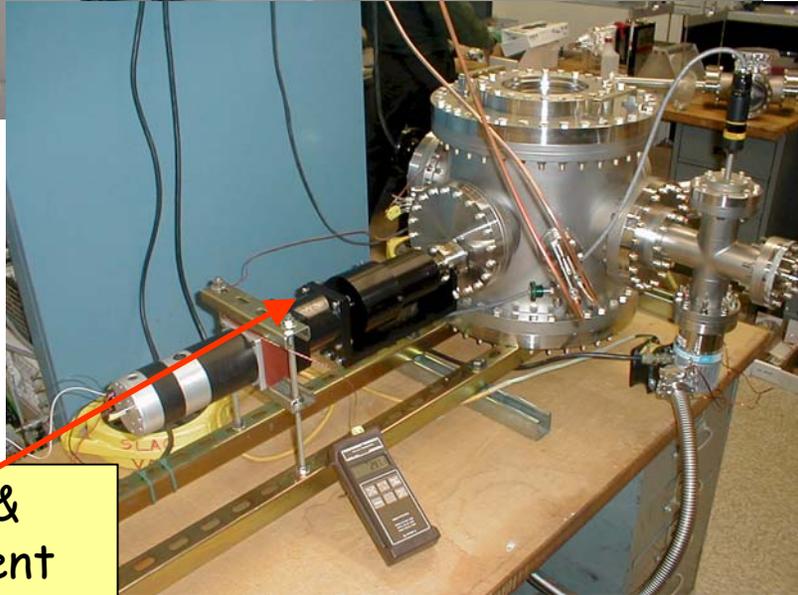
Renewable Spoiler Prototype Assembly



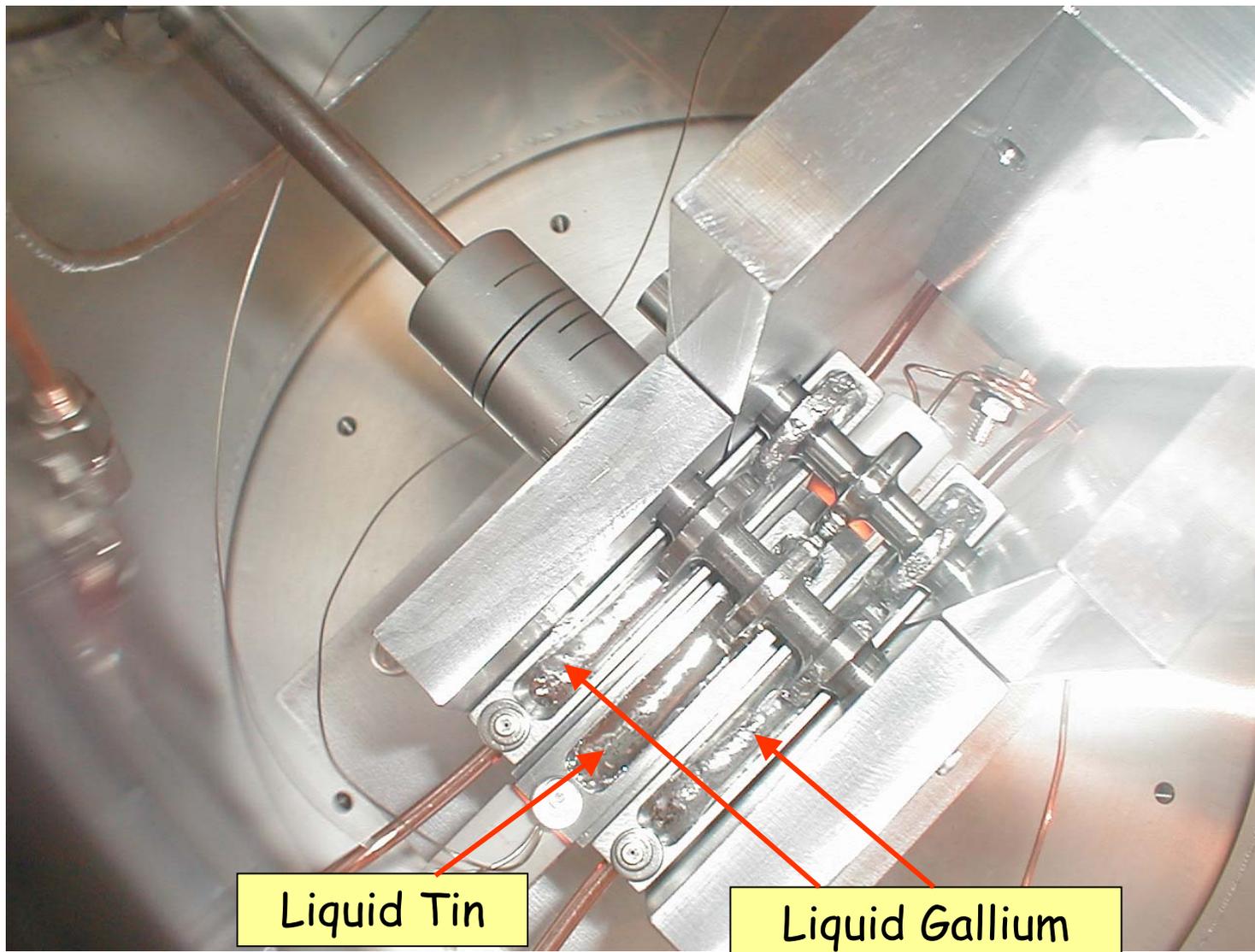
Niobium and Molybdenum Rotors



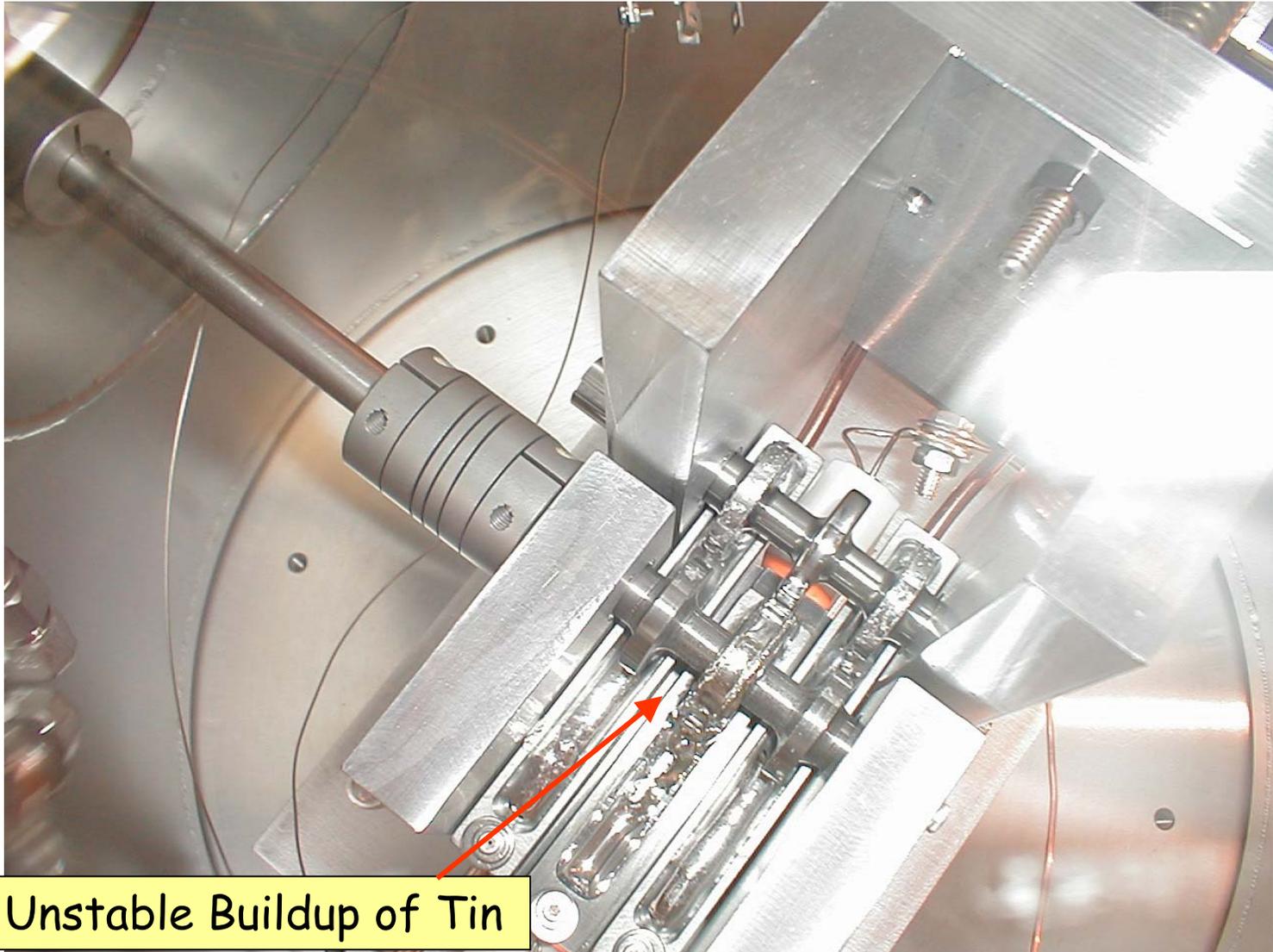
Vacuum vessel & Roller adjustment



Renewable Spoiler Operation



Spoiler with Thick Tin Coating



Unstable Buildup of Tin



Renewable Spoiler Status

Test Results

- Niobium roller (?) bearing fails after ~ 1 day operation. Vacuum pressure $\sim 2 \times 10^{-8}$ Torr.
- With relatively high operating temperature (~ 300 °C), a thin (visually estimated as a few $\times 100$ microns) Tin coating was produced. The surface finish of the coating was similar to that of the finishing roller.
- With relatively low operating temperature (~ 280 °C), a thick (>1 mm) coating of tin was produced. This coating was rolled to match the shape and finish of the finishing roller. This mode of operation was unstable, and within a minute all of the Tin solidified due to the increased heat leak.

Plans

- Replace roller bearings operating on Niobium with 400 series stainless bearings.
- Add a heated block to melt off the thick tin coating



Conclusions

- **Prototype rotary consumable spoiler constructed and works well**
 - NLC Baseline
 - Relatively minor modifications required for improved performance
- **Test system for investigations of more exotic liquid metal based renewable spoilers constructed. Seems do-able, but much more work required.**
- **R&D on hold as baseline design seems in hand and other projects require attention**